

REFERENCE: HB-0044

PROJECT: 50714

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STATE OF NORTH CAROLINA
DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT

STRUCTURE
SUBSURFACE INVESTIGATION

COUNTY ASHE

PROJECT DESCRIPTION REPLACE BRIDGE NO. 0093 ON
SR 1644 (MCNEIL ROAD) OVER NORTH FORK
NEW RIVER

SITE DESCRIPTION BRIDGE NO. 0093

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	HB-0044	1	

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THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF PREPARING THE SCOPE OF WORK TO BE INCLUDED IN THE REQUEST FOR PROPOSAL. THE VARIOUS FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N. C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT AT (919) 707-6850. THE SUBSURFACE PLANS AND REPORTS, FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA ARE NOT PART OF THE CONTRACT.

SOIL AND ROCK BOUNDARIES WITHIN A BOREHOLE ARE BASED ON GEOTECHNICAL INTERPRETATION UNLESS ENCOUNTERED IN A SAMPLE. INTERPRETED BOUNDARIES MAY NOT NECESSARILY REFLECT ACTUAL SUBSURFACE CONDITIONS BETWEEN SAMPLED STRATA AND BOREHOLE INFORMATION MAY NOT NECESSARILY REFLECT ACTUAL SUBSURFACE CONDITIONS BETWEEN BORINGS. THE LABORATORY SAMPLE DATA AND THE IN SITU (IN-PLACE) TEST DATA CAN BE RELIED ON ONLY TO THE DEGREE OF RELIABILITY INHERENT IN THE STANDARD TEST METHOD. THE OBSERVED WATER LEVELS OR SOIL MOISTURE CONDITIONS INDICATED IN THE SUBSURFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION. THESE WATER LEVELS OR SOIL MOISTURE CONDITIONS MAY VARY CONSIDERABLY WITH TIME ACCORDING TO CLIMATIC CONDITIONS INCLUDING TEMPERATURES, PRECIPITATION AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

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1. THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE N. C. DEPARTMENT OF TRANSPORTATION AS ACCURATE NOR IS IT CONSIDERED PART OF THE PLANS, SPECIFICATIONS OR CONTRACT FOR THE PROJECT.
2. BY HAVING REQUESTED THIS INFORMATION, THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

PERSONNEL

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K. CLARK

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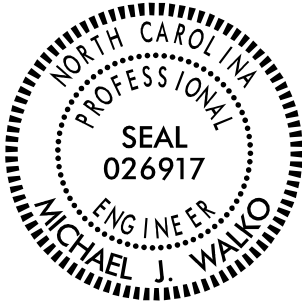
SUBMITTED BY CG2, PLLC

DATE DECEMBER, 2025

Prepared in the Office of:

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Signed by: Michael J. Walko 12/15/2025

42C02874D56441C SIGNATURE DATE

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UNLESS ALL SIGNATURES COMPLETED

NORTH CAROLINA DEPARTMENT OF TRANSPORTATION

DIVISION OF HIGHWAYS

GEOTECHNICAL ENGINEERING UNIT

SUBSURFACE INVESTIGATION

SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

SOIL DESCRIPTION										GRADATION										ROCK DESCRIPTION										TERMS AND DEFINITIONS									
SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 206, ASTM D1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE, <i>VERY STIFF, GRAY, SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6</i>										WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE. UNIFORMLY GRADED - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE. GAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.										HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED. AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL. THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:										ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER. AQUIFER - A WATER BEARING FORMATION OR STRATA. ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND. ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC. ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE. CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE. COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE. CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK. DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL. DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH. FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE. FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES. FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLOGGED FROM PARENT MATERIAL. FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM. FORMATION (FM.) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD. JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED. LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT. LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS. MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE. PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM. RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK. ROCK QUALITY DESIGNATION (RQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK. SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS. SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE. STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS (N OR BPF) OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS. STRATA CORE RECOVERY (SREC) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE. STRATA ROCK QUALITY DESIGNATION (SROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE. TOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.									
SOIL LEGEND AND AASHTO CLASSIFICATION										ANGULARITY OF GRAINS										WEATHERED ROCK (WR)										CRISTALLINE ROCK (CR)									
GENERAL CLASS.		GRANULAR MATERIALS (≤ 35% PASSING #200)					SILT-CLAY MATERIALS (> 35% PASSING #200)					ORGANIC MATERIALS					CRYSTALLINE ROCK (CR)		NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT N VALUES > 100 BLOWS PER FOOT IF TESTED.																				
GROUP CLASS.	A-1-a	A-1-b	A-3	A-2-4	A-2	A-2-6	A-2-7	A-4	A-5	A-6	A-7	A-1, A-2	A-3	A-4, A-5	A-6, A-7	FINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES GRANITE, GNEISS, GABBRO, SCHIST, ETC.																							
SYMBOL																FINE TO COARSE GRAIN METAMORPHIC AND NON-COASTAL PLAIN SEDIMENTARY ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES PHYLLITE, SLATE, SANDSTONE, ETC.																							
% PASSING	*10	50 MX	30 MX	50 MX	51 MN	10 MX	35 MX	35 MX	35 MX	35 MX	36 MN	36 MN	36 MN	36 MN	36 MN	COASTAL PLAIN SEDIMENTS CEMENTED INTO ROCK, BUT MAY NOT YIELD SPT REFUSAL. ROCK TYPE INCLUDES LIMESTONE, SANDSTONE, CEMENTED SHELL BEDS, ETC.																							
*40																																							
*200																																							
MATERIAL PASSING #40																																							
LL																																							
PI																																							
GROUP INDEX	0	0	0	0	4 MX	8 MX	12 MX	16 MX	NO MX																														
USUAL TYPES OF MAJOR MATERIALS	STONE FRAGS, GRAVEL, AND SAND	FINE SAND			SILTY OR CLAYEY GRAVEL AND SAND			SILTY SOILS								SOILS WITH LITTLE OR MODERATE AMOUNTS OF ORGANIC MATTER																							
GEN. RATING AS SUBGRADE	EXCELLENT TO GOOD					FAIR TO POOR					FAIR TO POOR	POOR	UNSATURABLE																										
PI OF A-7-5 SUBGROUP IS ≤ LL - 30; PI OF A-7-6 SUBGROUP IS > LL - 30																																							
CONSISTENCY OR DENSENESS										MISCELLANEOUS SYMBOLS										ROCK HARDNESS																			
PRIMARY SOIL TYPE		COMPACTNESS OR CONSISTENCY		RANGE OF STANDARD PENETRATION RESISTANCE (N-VALUE)				RANGE OF UNCONFINED COMPRESSIVE STRENGTH (TONS/FT ²)				ROADWAY EMBANKMENT (RE) WITH SOIL DESCRIPTION		25/025 DIP & DIP DIRECTION OF ROCK STRUCTURES		SLOPE INDICATOR INSTALLATION		SEVERE (SEV.)																					
GENERALLY GRANULAR MATERIAL (NON-COHESIVE)		VERY LOOSE LOOSE MEDIUM DENSE DENSE VERY DENSE		< 4 4 TO 10 10 TO 30 30 TO 50				N/A				SOIL SYMBOL		SPT DMT VST PMT TEST BORING		CONE PENETROMETER TEST		ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVIDENT BUT REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN. <i>IF TESTED, WOULD YIELD SPT N VALUES > 100 BPF</i>																					
GENERALLY SILT-CLAY MATERIAL (COHESIVE)		VERY SOFT SOFT MEDIUM STIFF STIFF VERY STIFF HARD		< 2 2 TO 4 4 TO 8 8 TO 15 15 TO 30 > 30				< 0.25 0.25 TO 0.5 0.5 TO 1.0 1 TO 2 2 TO 4 > 4				ARTIFICIAL FILL (AF) OTHER THAN ROADWAY EMBANKMENT		AUGER BORING		TEST BORING WITH CORE		VERY SEVERE (V SEV.)																					
												INFERRED SOIL BOUNDARY		CORE BORING		SOUNDING ROD		COMPLETE																					
												INFERRED ROCK LINE		MONITORING WELL																									
												ALLUVIAL SOIL BOUNDARY		PIEZOMETER INSTALLATION		SPT N-VALUE																							
TEXTURE OR GRAIN SIZE										RECOMMENDATION SYMBOLS										FRACTURE SPACING																			
U.S. STD. SIEVE SIZE OPENING (MM)		4 4.76		10 2.00		40 0.42		60 0.25		200 0.075		270 0.053		UNCLASSIFIED EXCAVATION - UNSUITABLE WASTE		UNCLASSIFIED EXCAVATION - ACCEPTABLE DEGRADABLE ROCK		UNCLASSIFIED EXCAVATION - ACCEPTABLE, BUT NOT TO BE USED IN THE TOP 3 FEET OF EMBANKMENT OR BACKFILL		VERY HARD																			
BOULDER (BLDR.)		COBBLE (COB.)		GRAVEL (GR.)		COARSE SAND (CSE, SD.)		FINE SAND (F SD.)		SILT (SL.)		CLAY (CL.)		SHALLOW UNDERCUT						HARD																			
GRAIN SIZE		305 12		75 3		2.0		0.25		0.05		0.005								MODERATELY HARD																			
SOIL MOISTURE - CORRELATION OF TERMS										ABBREVIATIONS										MEDIUM HARD																			
SOIL MOISTURE SCALE (ATTERBERG LIMITS)		FIELD MOISTURE DESCRIPTION		GUIDE FOR FIELD MOISTURE DESCRIPTION				AR - AUGER REFUSAL		MED. - MEDIUM MICA. - MICACEOUS MOD. - MODERATELY NP - NON PLASTIC ORG. - ORGANIC PMT - PRESSUREMETER TEST		VST - VANE SHEAR TEST		WEA. - WEATHERED		UNIT WEIGHT		DRY UNIT WEIGHT		SOFT																			
								CSE. - COARSE DMT - DILATOMETER TEST DPT - DYNAMIC PENETRATION TEST e - VOID RATIO F - FINE FOSS. - FOSSILIFEROUS FRAC. - FRACTURED, FRACTURES FRAGS. - FRAGMENTS HL. - HIGHLY		SD. - SAND, SANDY SL. - SILT, SILTY SIL. - SLIGHTLY TCR - TRICONE REFUSAL w - MOISTURE CONTENT V - VERY		S - BULK SS - SPLIT SPOON ST - SHELBY TUBE RS - ROCK RT - RECOMPACTED TRIAXIAL CBR - CALIFORNIA BEARING RATIO						MEDIUM HARD																					
PLASTICITY										EQUIPMENT USED ON SUBJECT PROJECT										SOFT																			
LL		LIQUID LIMIT		- SATURATED - (SAT.)				USUALLY LIQUID; VERY WET, USUALLY FROM BELOW THE GROUND WATER TABLE				DRILL UNITS:		ADVANCING TOOLS:		HAMMER TYPE:		CORE SIZE:		VERY WIDE																			
PL		PLASTIC LIMIT		- WET - (W)				SEMISOLID; REQUIRES DRYING TO ATTAIN OPTIMUM MOISTURE				CME-45C		CLAY BITS		X AUTOMATIC		H		WIDE																			
OM		OPTIMUM MOISTURE SHRINKAGE LIMIT		- MOIST - (M)				SOLID; AT OR NEAR OPTIMUM MOISTURE				CME-55		6" CONTINUOUS FLIGHT AUGER						MODERATELY CLOSE																			
SL				- DRY - (D)				REQUIRES ADDITIONAL WATER TO ATTAIN OPTIMUM MOISTURE				CME-550		8" HOLLOW AUGERS						CLOSE																			
												VANE SHEAR TEST		HARD FACED FINGER BITS						VERY CLOSE																			
												PORTABLE HOIST		TUNG.-CARBIDE INSERTS																									
												X DIEDRICH D-50		CASING X W/ ADVANCER																									
														TRICONE * STEEL TEETH																									
														TRICONE * TUNG.-CARB.																									
														CORE BIT																									

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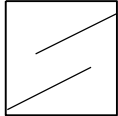
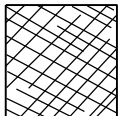
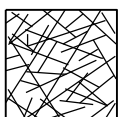
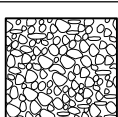
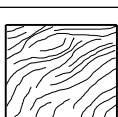
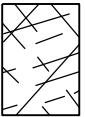
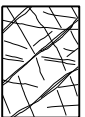
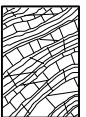
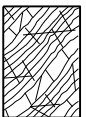
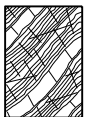
SUBSURFACE INVESTIGATION

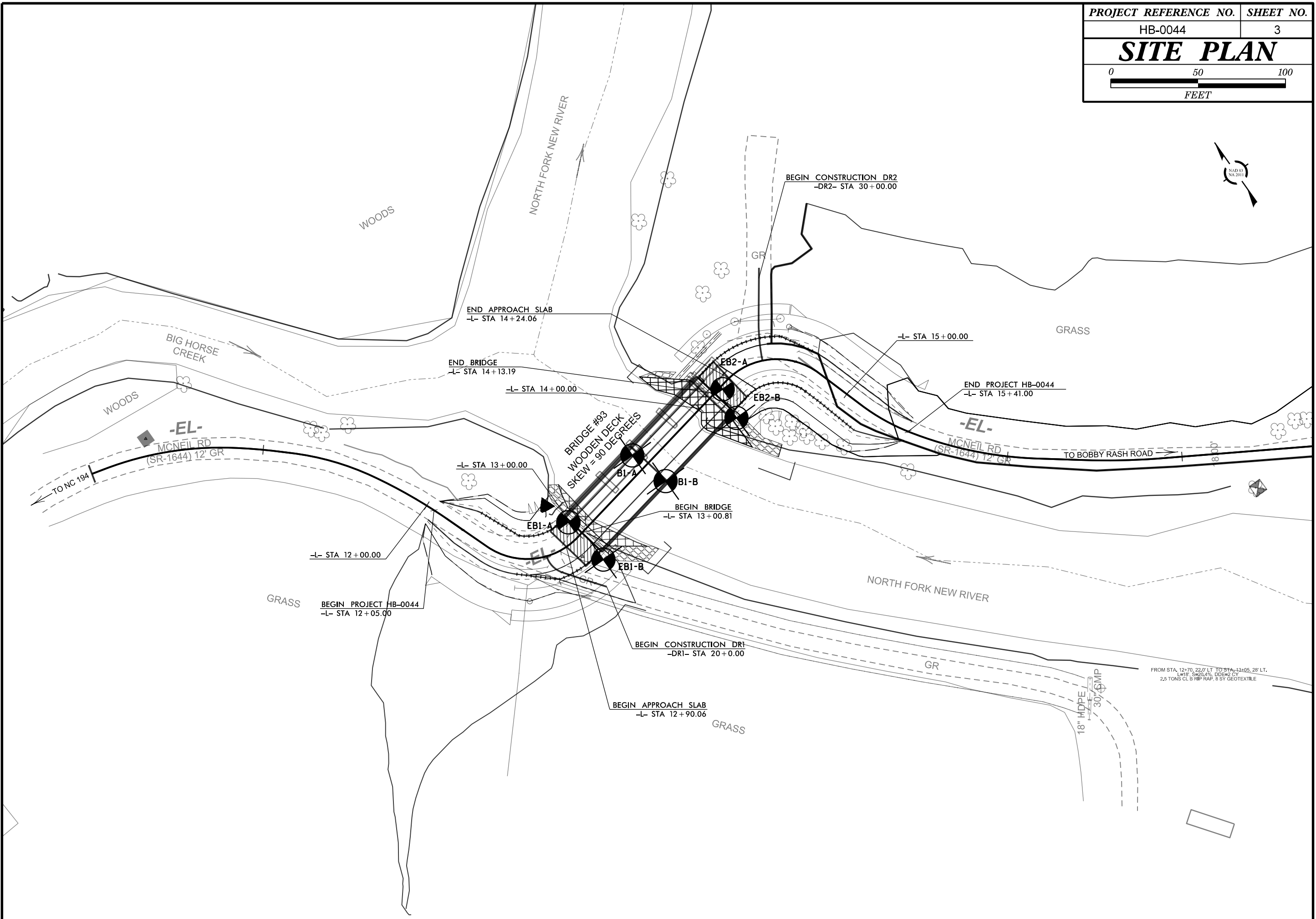
SUPPLEMENTAL LEGEND, GEOLOGICAL STRENGTH INDEX (GSI) TABLES

FROM AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS

AASHTO LRFD Figure 10.4.6.4-1 — Determination of GSI for Jointed Rock Mass (Marinos and Hoek, 2000)

AASHTO LRFD Figure 10.4.6.4-2 — Determination of GSI for Tectonically Deformed Heterogeneous Rock Masses (Marinos and Hoek, 2000)

GEOLOGICAL STRENGTH INDEX (GSI) FOR JOINTED ROCKS (Hoek and Marinos, 2000) From the lithology, structure and surface conditions of the discontinuities, estimate the average value of GSI. Do not try to be too precise. Quoting a range from 33 to 37 is more realistic than stating that GSI = 35. Note that the table does not apply to structurally controlled failures. Where weak planar structural planes are present in an unfavorable orientation with respect to the excavation face, these will dominate the rock mass behaviour. The shear strength of surfaces in rocks that are prone to deterioration as a result of changes in moisture content will be reduced if water is present. When working with rocks in the fair to very poor categories, a shift to the right may be made for wet conditions. Water pressure is dealt with by effective stress analysis.	SURFACE CONDITIONS VERY GOOD Very rough, fresh unweathered surfaces GOOD Rough, slightly weathered, iron stained surfaces FAIR Smooth, moderately weathered and altered surfaces POOR Slickensided, highly weathered surfaces with compact coatings or fillings or angular fragments VERY POOR Slickensided, highly weathered surfaces with soft clay coatings or fillings	GSI FOR HETEROGENEOUS ROCK MASSES SUCH AS FLYSCH (Marinos, P and Hoek E., 2000) From a description of the lithology, structure and surface conditions (particularly of the bedding planes), choose a box in the chart. Locate the position in the box that corresponds to the condition of the discontinuities and estimate the average value of GSI from the contours. Do not attempt to be too precise. Quoting a range from 33 to 37 is more realistic than giving GSI = 35. Note that the Hoek-Brown criterion does not apply to structurally controlled failures. Where unfavourably oriented continuous weak planar discontinuities are present, these will dominate the behaviour of the rock mass. The strength of some rock masses is reduced by the presence of groundwater and this can be allowed for by a slight shift to the right in the columns for fair, poor and very poor conditions. Water pressure does not change the value of GSI and it is dealt with by using effective stress analysis.	SURFACE CONDITIONS OF DISCONTINUITIES (Predominantly bedding planes) VERY GOOD - Very Rough, fresh unweathered surfaces GOOD - Rough, slightly weathered surfaces FAIR - Smooth, moderately weathered and altered surfaces POOR - Very smooth, occasionally slickensided surfaces with compact coatings or fillings with angular fragments VERY POOR - Very smooth, slickensided or highly weathered surfaces with soft clay coatings or fillings
STRUCTURE INTACT OR MASSIVE - intact rock specimens or massive in situ rock with few widely spaced discontinuities BLOCKY - well interlocked undisturbed rock mass consisting of cubical blocks formed by three intersecting discontinuity sets VERY BLOCKY - interlocked, partially disturbed mass with multi-faceted angular blocks formed by 4 or more joint sets BLOCKY/DISTURBED/SEAMY - folded with angular blocks formed by many intersecting discontinuity sets. Persistence of bedding planes or schistosity DISINTEGRATED - poorly interlocked, heavily broken rock mass with mixture of angular and rounded rock pieces LAMINATED/SHEARED - Lack of blockiness due to close spacing of weak schistosity or shear planes	DECREASING INTERLOCKING OF ROCK PIECES 90 80 70 60 50 40 30 20 10 N/A N/A	COMPOSITION AND STRUCTURE A. Thick bedded, very blocky sandstone The effect of pelitic coatings on the bedding planes is minimized by the confinement of the rock mass. In shallow tunnels or slopes these bedding planes may cause structurally controlled instability. B. Sandstone with thin inter-layers of siltstone C. Sandstone and siltstone in similar amounts D. Siltstone or silty shale with sandstone layers E. Weak siltstone or clayey shale with sandstone layers C, D, E, and G - may be more or less folded than illustrated but this does not change the strength. Tectonic deformation, faulting and loss of continuity moves these categories to F and H. F. Tectonically deformed, intensively folded/faulted, sheared clayey shale or siltstone with broken and deformed sandstone layers forming an almost chaotic structure G. Undisturbed silty or clayey shale with or without a few very thin sandstone layers H. Tectonically deformed silty or clayey shale forming a chaotic structure with pockets of clay. Thin layers of sandstone are transformed into small rock pieces.	70 60 50 40 30 20 10



GEOTECHNICAL BORING REPORT
BORE LOG

WBS 50714.1.1			TIP HB-0044			COUNTY ASHE			GEOLOGIST M. Malisher							
SITE DESCRIPTION Replace Bridge No. 093 on SR 1644 (McNeil Road) over North Fork New River								GROUND WTR (ft)								
BORING NO. EB1-A			STATION 13+01			OFFSET 10 ft LT		ALIGNMENT -L-		0 HR. N/A						
COLLAR ELEV. 2,630.4 ft			TOTAL DEPTH 8.8 ft			NORTHING 1,004,823		EASTING 1,266,806		24 HR. FIAD						
DRILL RIG/HAMMER EFF./DATE CG20446 Diedrich D-50 97% 04/30/2024						DRILL METHOD NW Casing w/ SPT			HAMMER TYPE Automatic							
DRILLER C. Odom			START DATE 11/18/25			COMP. DATE 11/18/25			SURFACE WATER DEPTH N/A							
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	MOI	L O G	SOIL AND ROCK DESCRIPTION		
			0.5ft	0.5ft	0.5ft	0	25	50	75	100				ELEV. (ft)	DEPTH (ft)	
2635																
2630	2,629.5	0.9	4	21	16									2,630.4	GROUND SURFACE	0.0
	2,629.5													2,629.5	ROADWAY EMBANKMENT	0.9
	2,626.9	3.5	WOH	1	1									2,627.4	ALLUVIAL	3.0
2625														Dense, Brown-Gray-Black, Fine to Coarse Sandy GRAVEL (A-1-a)		
														Soft, Gray, Fine Sandy SILT (A-4), with trace mica		
	2,621.6	8.8	60/0.0											2,621.6		8.8
														Boring Terminated with Standard Penetration Test Refusal at Elevation 2,621.6 ft On Crystalline Rock (Biotite Granitic Gneiss)		

NCDOT BORE DOUBLE 04_GEO_BRDG93_GTM.GPJ NC_DOT.GDT 12/10/25

GEOTECHNICAL BORING REPORT
BORE LOG

WBS 50714.1.1				TIP HB-0044		COUNTY ASHE		GEOLOGIST K. Clark							
SITE DESCRIPTION Replace Bridge No. 093 on SR 1644 (McNeil Road) over North Fork New River											GROUND WTR (ft)				
BORING NO. EB1-B			STATION 12+99			OFFSET 19 ft RT			ALIGNMENT -L-		0 HR.	N/A			
COLLAR ELEV. 2,635.1 ft			TOTAL DEPTH 20.1 ft			NORTHING 1,004,794			EASTING 1,266,810		24 HR.	9.7			
DRILL RIG/HAMMER EFF./DATE CG20446 Diedrich D-50 97% 04/30/2024						DRILL METHOD NW Casing W/SPT & Core				HAMMER TYPE Automatic					
DRILLER C. Odom			START DATE 10/20/25			COMP. DATE 10/20/25			SURFACE WATER DEPTH N/A						
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION	
			0.5ft	0.5ft	0.5ft	0	25	50	75	100				ELEV. (ft)	DEPTH (ft)
2640															
2635	2,635.1	0.0												2,635.1	0.0
2630	2,630.7	4.4	1	1	3	4					M			GROUND SURFACE	
2625	2,625.7	9.4	2	1	1	2					M			ALLUVIAL	
	2,624.0	11.1												Soft, Brown-Red, Fine Sandy SILT (A-4), with trace mica and organics	
2620														RESIDUAL	
														Dense, Gray, Silty Fine SAND (A-2-4), with trace mica and gravel-sized rock fragments	
2615														CRYSTALLINE ROCK	
														Gray-White, (Biotite Granitic Gneiss)	
														REC: 94%	
														RQD: 86%	
														GSI: 65-70	

NCDOT BORE DOUBLE 04_GEO_BRDG93_GTM.GPJ NC_DOT.GDT 12/10/25

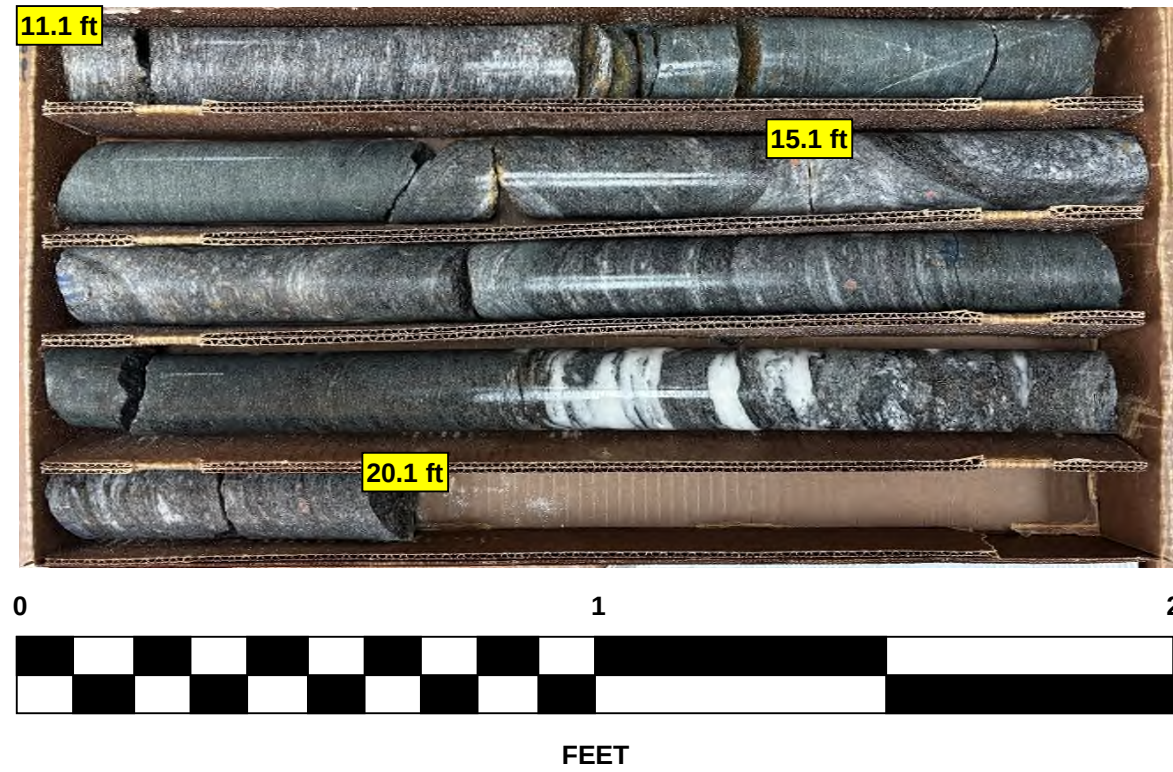
GEOTECHNICAL BORING REPORT
CORE LOG

SHEET 5

WBS 50714.1.1				TIP HB-0044		COUNTY ASHE		GEOLOGIST K. Clark			
SITE DESCRIPTION Replace Bridge No. 093 on SR 1644 (McNeil Road) over North Fork New River										GROUND WTR (ft)	
BORING NO. EB1-B				STATION 12+99			OFFSET 19 ft RT		ALIGNMENT -L-		0 HR. N/A
COLLAR ELEV. 2,635.1 ft				TOTAL DEPTH 20.1 ft			NORTHING 1,004,794		EASTING 1,266,810		24 HR. 9.7
DRILL RIG/HAMMER EFF./DATE CG20446 Diedrich D-50 97% 04/30/2024							DRILL METHOD NW Casing W/SPT & Core			HAMMER TYPE Automatic	
DRILLER C. Odom				START DATE 10/20/25			COMP. DATE 10/20/25		SURFACE WATER DEPTH N/A		
CORE SIZE NQ				TOTAL RUN 9.0 ft							
ELEV (ft)	RUN ELEV (ft)	DEPTH (ft)	RUN (ft)	DRILL RATE (Min/ft)	RUN REC. (ft) % RQD (ft) %		SAMP. NO.	STRATA REC. (ft) % RQD (ft) %		LOG	DESCRIPTION AND REMARKS
											ELEV. (ft) DEPTH (ft)
2624											Begin Coring @ 11.1 ft
	2,624.0	11.1	4.0	N=60/0.0 3:06/1.0 3:51/1.0 2:28/1.0 3:25/1.0	(3.5) 88%	(2.7) 68%		(8.5) 94%	(7.7) 86%		2,624.0 11.1 CRYSTALLINE ROCK Moderately to Very Slightly Weathered, Hard to Very Hard, Gray-White, (Biotite Granitic Gneiss), with Very Close to Moderately Close Fracture Spacing
2620	2,620.0	15.1									
			5.0	2:37/1.0 2:50/1.0 3:04/1.0 2:45/1.0 2:00/1.0	(5.0) 100%	(5.0) 100%					GSI: 65-70
2615	2,615.0	20.1									2,615.0 20.1 Boring Terminated at Elevation 2,615.0 ft In Crystalline Rock (Biotite Granitic Gneiss)

NCDOT BORE DOUBLE 04_GEO_BRDG93_GTM.GPJ NC_DOT.GDT 12/10/25

Replace Bridge No. 93 on SR 1644 (McNeil Road) over
North Fork New River
Ashe County, North Carolina
Rock Core Photographs
EB1-B
11.1 to 20.1 Feet



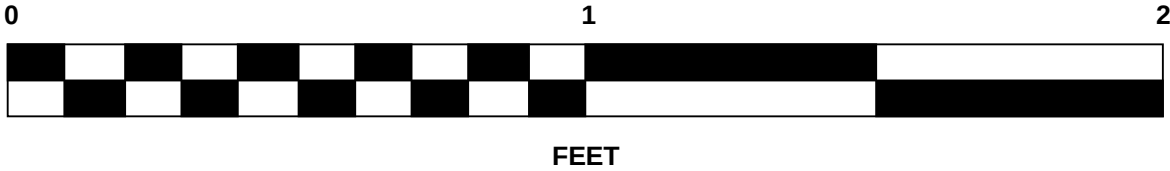
GEOTECHNICAL BORING REPORT

CORE LOG

NCDOT CORE DOUBLE 04 GEO BRDG93 GTM.GPJ NC DOT.GDT 12/11/25

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Replace Bridge No. 93 on SR 1644 (McNeil Road) over
North Fork New River
Ashe County, North Carolina
Rock Core Photographs
B1-A
2.5 to 17.5 Feet



GEOTECHNICAL BORING REPORT
BORE LOG

WBS 50714.1.1			TIP HB-0044			COUNTY ASHE			GEOLOGIST M. Malisher					
SITE DESCRIPTION Replace Bridge No. 093 on SR 1644 (McNeil Road) over North Fork New River									GROUND WTR (ft)					
BORING NO. B1-B			STATION 13+56			OFFSET 14 ft RT			ALIGNMENT -L-			0 HR. N/A		
COLLAR ELEV. 2,625.1 ft			TOTAL DEPTH 30.1 ft			NORTHING 1,004,810			EASTING 1,266,865			24 HR. Caved		
DRILL RIG/HAMMER EFF./DATE CG20446 Diedrich D-50 97% 04/30/2024						DRILL METHOD NW Casing W/SPT & Core			HAMMER TYPE Automatic					
DRILLER C. Odom			START DATE 10/16/25			COMP. DATE 10/16/25			SURFACE WATER DEPTH 0.4ft					
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG	SOIL AND ROCK DESCRIPTION	DEPTH (ft)
			0.5ft	0.5ft	0.5ft	0	25	50	75	100				
2630														
2625	2,625.1	0.0												
			5	5	11									
2620	2,621.1	4.0	60/0.0											
	2,619.5	5.6	60/0.0											
2615														
2610														
2605														
2600														
2595														
Boring Terminated at Elevation 2,595.0 ft In Crystalline Rock (Biotite Granitic Gneiss)														

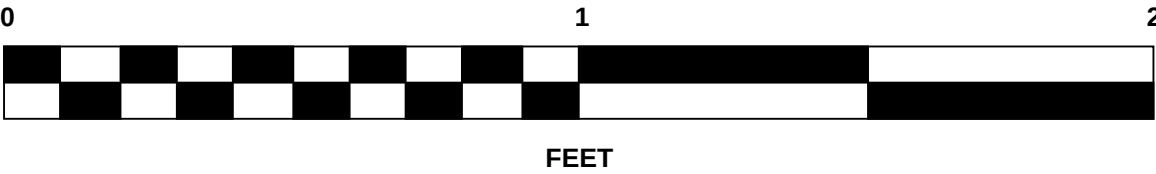
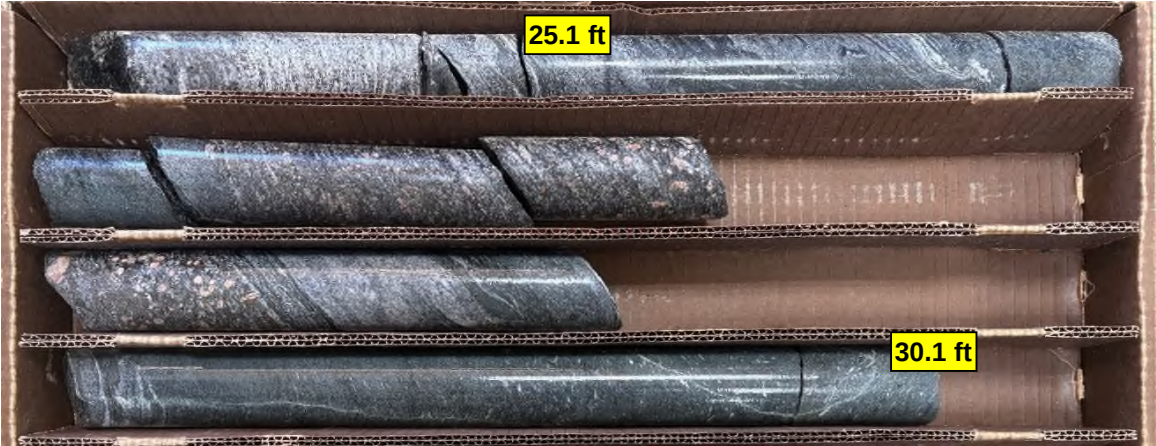
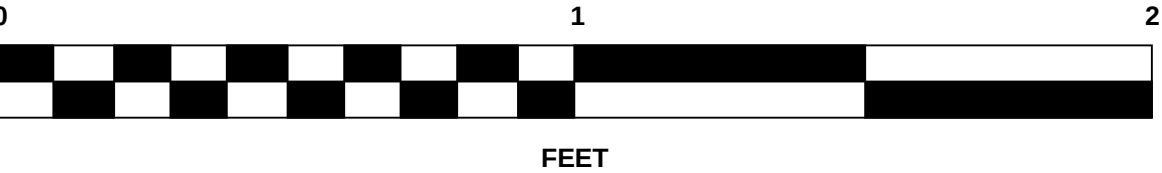
NCDOT BORE DOUBLE 04_GEO_BRDG93_GTM.GPJ NC_DOT.GDT 12/11/25

GEOTECHNICAL BORING REPORT
CORE LOG

WBS 50714.1.1				TIP HB-0044				COUNTY ASHE				GEOLOGIST M. Malisher							
SITE DESCRIPTION Replace Bridge No. 093 on SR 1644 (McNeil Road) over North Fork New River												GROUND WTR (ft)							
BORING NO. B1-B				STATION 13+56				OFFSET 14 ft RT				ALIGNMENT -L-				0 HR. N/A			
COLLAR ELEV. 2,625.1 ft				TOTAL DEPTH 30.1 ft				NORTHING 1,004,810				EASTING 1,266,865				24 HR. Caved			
DRILL RIG/HAMMER EFF./DATE CG20446 Diedrich D-50 97% 04/30/2024								DRILL METHOD NW Casing W/SPT & Core				HAMMER TYPE Automatic							
DRILLER C. Odom				START DATE 10/16/25				COMP. DATE 10/16/25				SURFACE WATER DEPTH 0.4ft							
CORE SIZE NQ				TOTAL RUN 24.5 ft															
ELEV (ft)	RUN ELEV (ft)	DEPTH (ft)	RUN (ft)	DRILL RATE (Min/ft)	RUN REC. (ft) % RQD (ft) %		SAMP. NO.	STRATA REC. (ft) % RQD (ft) %		L O G	DESCRIPTION AND REMARKS					DEPTH (ft)			
2619.5											Begin Coring @ 5.6 ft								
	2,619.5	5.6	4.5	N=60/0.0 2:16/1.0 2:17/1.0 1:54/1.0 1:33/1.0 0:57/0.5	(4.5) 100%	(0.8) 18%		(24.4) 100%	(10.5) 43%		2,619.5	Moderately Weathered to Fresh, Moderately Hard to Hard, Gray-White-Black, (Biotite Granitic Gneiss), with Very Close to Moderately Close Fracture Spacing					5.6		
2615	2,615.0	10.1											GSI: 35-40						
			5.0	1:50/1.0 1:10/1.0 1:21/1.0 1:28/1.0 1:40/1.0	(5.0) 100%	(0.5) 10%													
2610	2,610.0	15.1																	
			5.0	1:53/1.0 2:35/1.0 1:35/1.0 1:41/1.0 1:25/1.0	(5.0) 100%	(2.4) 48%													
2605	2,605.0	20.1																	
			5.0	1:13/1.0 1:33/1.0 2:07/1.0 2:15/1.0 3:15/1.0	(5.0) 100%	(2.6) 52%													
2600	2,600.0	25.1																	
			5.0	2:24/1.0 2:13/1.0 2:07/1.0 4:18/1.0 5:12/1.0	(4.9) 98%	(4.2) 84%													
2595	2,595.0	30.1									2,595.0	Boring Terminated at Elevation 2,595.0 ft In Crystalline Rock (Biotite Granitic Gneiss)					30.1		

NCDOT CORE DOUBLE 04_GEO_BRDG93_GTM.GPJ NC_DOT.GDT 12/11/25

Replace Bridge No. 93 on SR 1644 (McNeil Road) over
North Fork New River
Ashe County, North Carolina
Rock Core Photographs
B1-B
5.6 to 30.1 Feet



GEOTECHNICAL BORING REPORT
BORE LOG

WBS 50714.1.1			TIP HB-0044			COUNTY ASHE			GEOLOGIST M. Malisher						
SITE DESCRIPTION Replace Bridge No. 093 on SR 1644 (McNeil Road) over North Fork New River									GROUND WTR (ft)						
BORING NO. EB2-A			STATION 14+17			OFFSET 2 ft RT			ALIGNMENT -L-						
COLLAR ELEV. 2,628.6 ft			TOTAL DEPTH 7.2 ft			NORTHING 1,004,834			EASTING 1,266,922						
DRILL RIG/HAMMER EFF./DATE CG20446 Diedrich D-50 97% 04/30/2024						DRILL METHOD NW Casing w/ SPT			HAMMER TYPE Automatic						
DRILLER C. Odom			START DATE 11/18/25			COMP. DATE 11/18/25			SURFACE WATER DEPTH N/A						
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	MOI	L O G	SOIL AND ROCK DESCRIPTION	DEPTH (ft)
			0.5ft	0.5ft	0.5ft	0	25	50	75	100					
2630															
	2,628.6	0.0	2	2	2									2,628.6	GROUND SURFACE 0.0
2625	2,625.6	3.0	3	4	5							Sat.		ALLUVIAL Loose, Brown-Black, Fine to Coarse Gravelly SAND (A-1-b)	
	2,621.4	7.2										Sat.		2,621.4	7.2
Boring Terminated with Standard Penetration Test Refusal at Elevation 2,621.4 ft On Crystalline Rock (Biotite Granitic Gneiss)															

NCDOT BORE DOUBLE 04_GEO_BRDG93_GTM.GPJ NC_DOT.GDT 12/10/25

GEOTECHNICAL BORING REPORT

BORE LOG

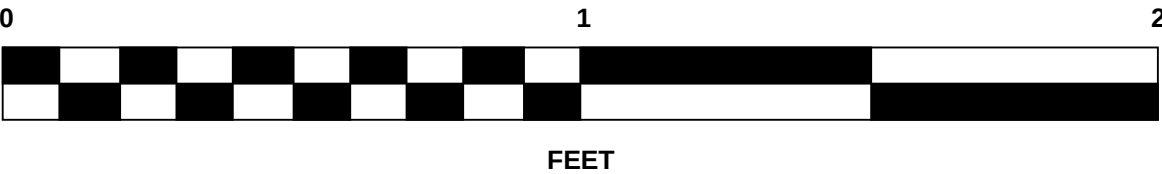
WBS 50714.1.1			TIP HB-0044			COUNTY ASHE			GEOLOGIST M. Malisher							
SITE DESCRIPTION Replace Bridge No. 093 on SR 1644 (McNeil Road) over North Fork New River									GROUND WTR (ft)							
BORING NO. EB2-B			STATION 14+11			OFFSET 19 ft RT			ALIGNMENT -L-			0 HR. N/A				
COLLAR ELEV. 2,631.0 ft			TOTAL DEPTH 14.6 ft			NORTHING 1,004,816			EASTING 1,266,919			24 HR. 5.0				
DRILL RIG/HAMMER EFF./DATE CG20446 Diedrich D-50 97% 04/30/2024						DRILL METHOD NW Casing W/SPT & Core			HAMMER TYPE Automatic							
DRILLER C. Odom			START DATE 10/17/25			COMP. DATE 10/17/25			SURFACE WATER DEPTH N/A							
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION		
			0.5ft	0.5ft	0.5ft	0	25	50	75	100				ELEV. (ft)	DEPTH (ft)	
2635																
2630	2,631.0	0.0	1	2	2									2,631.0	0.0	
	2,627.7	3.3	4	3	3											
2625																
	2,622.7	8.3												2,622.7	8.3	
2620	2,621.0	10.0	100/0.2			100/0.2								2,621.0	10.0	
			60/0.0			60/0.0										
														2,616.4	14.6	
															REC: 98%	
															RQD: 76%	
															GSI: 55-60	
															Boring Terminated at Elevation 2,616.4 ft In Crystalline Rock (Biotite Granitic Gneiss)	
															Surficial Organic Soil - 0.2'	

GEOTECHNICAL BORING REPORT

CORE LOG

WBS 50714.1.1				TIP HB-0044		COUNTY ASHE		GEOLOGIST M. Malisher					
SITE DESCRIPTION Replace Bridge No. 093 on SR 1644 (McNeil Road) over North Fork New River										GROUND WTR (ft)			
BORING NO. EB2-B				STATION 14+11		OFFSET 19 ft RT		ALIGNMENT -L-		0 HR. N/A			
COLLAR ELEV. 2,631.0 ft				TOTAL DEPTH 14.6 ft		NORTHING 1,004,816		EASTING 1,266,919		24 HR. 5.0			
DRILL RIG/HAMMER EFF./DATE CG20446 Diedrich D-50 97% 04/30/2024						DRILL METHOD NW Casing W/SPT & Core			HAMMER TYPE Automatic				
DRILLER C. Odom				START DATE 10/17/25		COMP. DATE 10/17/25		SURFACE WATER DEPTH N/A					
CORE SIZE NQ				TOTAL RUN 4.6 ft									
ELEV (ft)	RUN ELEV (ft)	DEPTH (ft)	RUN (ft)	DRILL RATE (Min/ft)	RUN REC. (ft) % ROD (ft) %		SAMP. NO.	STRATA REC. (ft) % ROD (ft) %		L O G	DESCRIPTION AND REMARKS	DEPTH (ft)	
2621											Begin Coring @ 10.0 ft		
2620	2,621.0	10.0	4.6	N=60/0.0 4:25/1.0 2:45/1.0 3:03/1.0 3:12/1.0 1:47/0.6	(4.5) 98%	(3.5) 76%		(4.5) 98%	(3.5) 76%		2,621.0	CRYSTALLINE ROCK	10.0
	2,616.4	14.6									2,616.4	Slightly Weathered to Fresh, Hard, Gray-White, (Biotite Granitic Gneiss), with Very Close to Moderately Close Fracture Spacing	14.6
											GSi: 55-60		
											Boring Terminated at Elevation 2,616.4 ft In Crystalline Rock (Biotite Granitic Gneiss)		
											Surficial Organic Soil - 0.2'		

Replace Bridge No. 93 on SR 1644 (McNeil Road) over
North Fork New River
Ashe County, North Carolina
Rock Core Photographs
EB2-B
10.0 to 14.6 Feet



ROCK TEST RESULTS									
SAMPLE NO.	BORING	NORTHING	EASTING	STATION	OFFSET	DEPTH INTERVAL	ROCK TYPE	UNIT WEIGHT (PCF)	UNCONFINED COMPRESSIVE STRENGTH
RS-01	B1-A	1004833	1266858	13+54 -L-	10' LT	10.2'-10.7'	BIOTITE GRANITIC GNEISS	178.2	8,310 psi /1,197 ksf

Alex M. Atkinson

AUTHORIZED SIGNATURE
NCDOT CERT NO. 130-04-0212

Prepared in the Office of:
F&ME CONSULTANTS, INC.
COLUMBIA, SOUTH CAROLINA
NCDOT LAB CERT. NO. 130-0212



PHOTO #1: VIEW FROM END BENT NO. 1 FACING EAST TOWARD END BENT NO. 2.



PHOTO #2: VIEW FROM END BENT NO. 2 FACING NORTH, DOWNSTREAM.

REFERENCE: HB-0050

PROJECT: 50720

CONTENTS

SHEET NO.	DESCRIPTION
1	TITLE SHEET
2	LEGEND (SOIL & ROCK)
2A	SUPPLEMENTAL LEGEND (GSI)
3	SITE PLAN
4-13	BORE LOGS, CORE REPORTS, & CORE PHOTOS
14	ROCK TEST RESULTS
15	SITE PHOTOGRAPHS

STATE OF NORTH CAROLINA
DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT

STRUCTURE
SUBSURFACE INVESTIGATION

COUNTY ASHE
PROJECT DESCRIPTION REPLACE BRIDGE NO. 463 ON
SR 1563 (CLIFFTON ROAD) OVER NORTH FORK
NEW RIVER
SITE DESCRIPTION BRIDGE NO. 0463

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	HB-0050	1	

CAUTION NOTICE

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLANNING AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N.C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT, AT (919) 707-6850. THE SUBSURFACE PLANS AND REPORTS, FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA ARE NOT PART OF THE CONTRACT.

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- NOTES:
- THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE N.C. DEPARTMENT OF TRANSPORTATION AS ACCURATE NOR IS IT CONSIDERED PART OF THE PLANS, SPECIFICATIONS OR CONTRACT FOR THE PROJECT.
 - BY HAVING REQUESTED THIS INFORMATION, THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

PERSONNEL

CG2 EXPLORATION

P. MCKENZIE

M. MALISHER

INVESTIGATED BY CG2, PLLC

DRAWN BY M. MALISHER, E.I.T.

CHECKED BY M. WALKO, P.E.

SUBMITTED BY CG2, PLLC

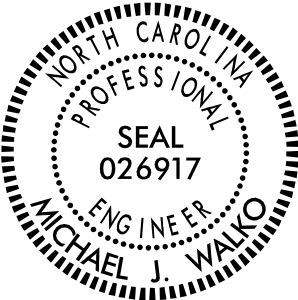
DATE DECEMBER, 2025

Prepared in the Office of:



CAROLINAS
GEOTECHNICAL
GROUP

1805 SARDIS ROAD N
SUITE 100
CHARLOTTE, NC 28270
(980) 339-8684



Signed by: Michael J. Walko 12/15/2025

42C082874D56441C SIGNATURE DATE

DOCUMENT NOT CONSIDERED FINAL
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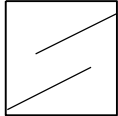
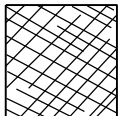
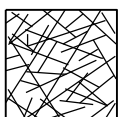
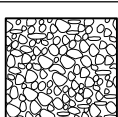
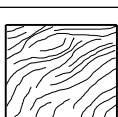
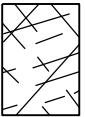
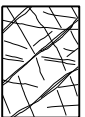
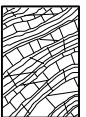
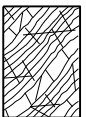
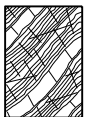
NORTH CAROLINA DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT

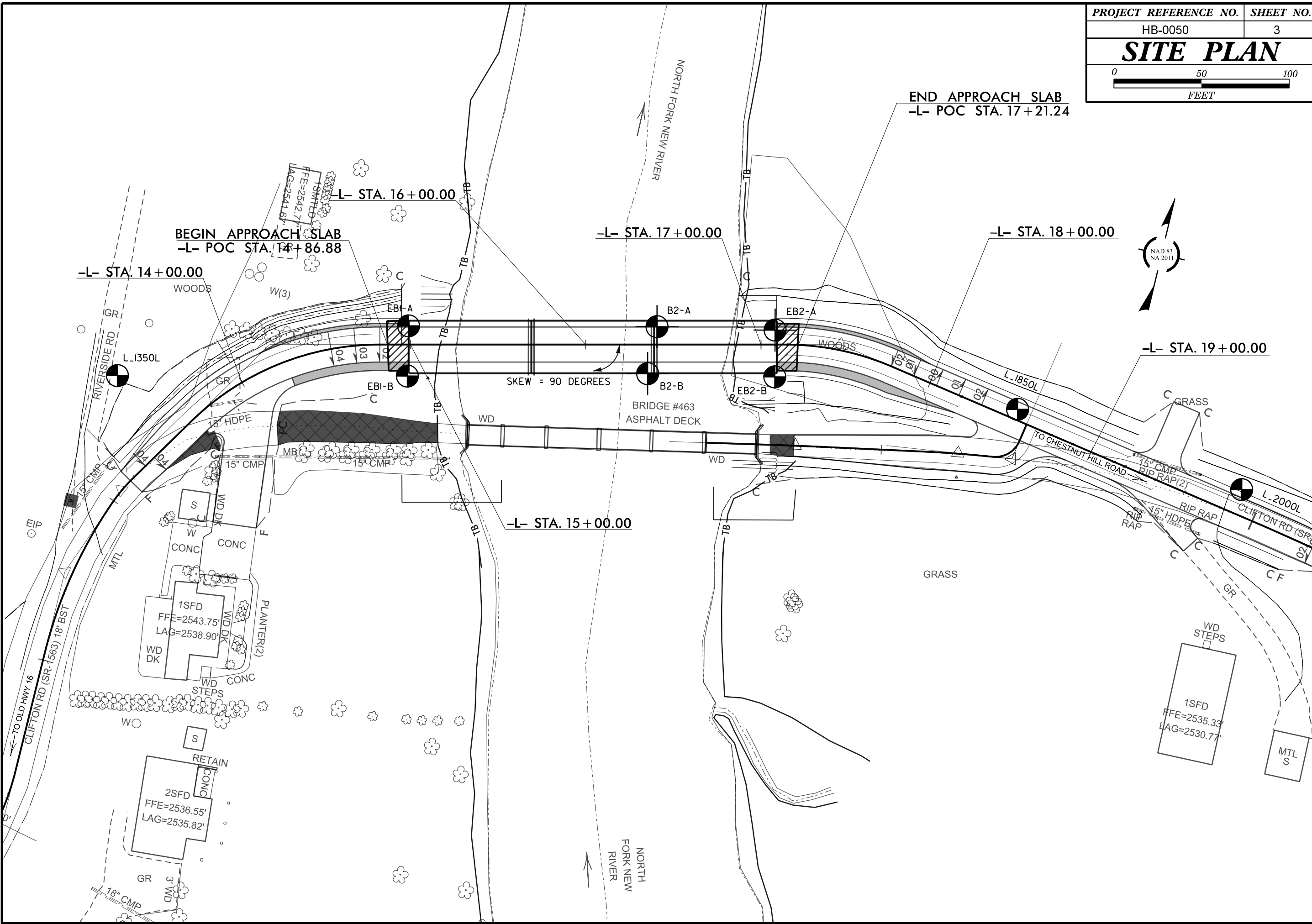
SUBSURFACE INVESTIGATION

SUPPLEMENTAL LEGEND, GEOLOGICAL STRENGTH INDEX (GSI) TABLES
FROM AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS

AASHTO LRFD Figure 10.4.6.4-1 — Determination of GSI for Jointed Rock Mass (Marinos and Hoek, 2000)

AASHTO LRFD Figure 10.4.6.4-2 — Determination of GSI for Tectonically Deformed Heterogeneous Rock Masses (Marinos and Hoek, 2000)

GEOLOGICAL STRENGTH INDEX (GSI) FOR JOINTED ROCKS (Hoek and Marinos, 2000) From the lithology, structure and surface conditions of the discontinuities, estimate the average value of GSI. Do not try to be too precise. Quoting a range from 33 to 37 is more realistic than stating that GSI = 35. Note that the table does not apply to structurally controlled failures. Where weak planar structural planes are present in an unfavorable orientation with respect to the excavation face, these will dominate the rock mass behaviour. The shear strength of surfaces in rocks that are prone to deterioration as a result of changes in moisture content will be reduced if water is present. When working with rocks in the fair to very poor categories, a shift to the right may be made for wet conditions. Water pressure is dealt with by effective stress analysis.	SURFACE CONDITIONS VERY GOOD Very rough, fresh unweathered surfaces GOOD Rough, slightly weathered, iron stained surfaces FAIR Smooth, moderately weathered and altered surfaces POOR Slickensided, highly weathered surfaces with compact coatings or fillings or angular fragments VERY POOR Slickensided, highly weathered surfaces with soft clay coatings or fillings	STRUCTURE INTACT OR MASSIVE - intact rock specimens or massive in situ rock with few widely spaced discontinuities BLOCKY - well interlocked undisturbed rock mass consisting of cubical blocks formed by three intersecting discontinuity sets VERY BLOCKY - interlocked, partially disturbed mass with multi-faceted angular blocks formed by 4 or more joint sets BLOCKY/DISTURBED/SEAMY - folded with angular blocks formed by many intersecting discontinuity sets. Persistence of bedding planes or schistosity DISINTEGRATED - poorly interlocked, heavily broken rock mass with mixture of angular and rounded rock pieces LAMINATED/SHEARED - Lack of blockiness due to close spacing of weak schistosity or shear planes	DECREASING SURFACE QUALITY ➡ 90 80 70 60 50 40 30 20 10 N/A N/A	GSI FOR HETEROGENEOUS ROCK MASSES SUCH AS FLYSCH (Marinos, P and Hoek E., 2000) From a description of the lithology, structure and surface conditions (particularly of the bedding planes), choose a box in the chart. Locate the position in the box that corresponds to the condition of the discontinuities and estimate the average value of GSI from the contours. Do not attempt to be too precise. Quoting a range from 33 to 37 is more realistic than giving GSI = 35. Note that the Hoek-Brown criterion does not apply to structurally controlled failures. Where unfavourably oriented continuous weak planar discontinuities are present, these will dominate the behaviour of the rock mass. The strength of some rock masses is reduced by the presence of groundwater and this can be allowed for by a slight shift to the right in the columns for fair, poor and very poor conditions. Water pressure does not change the value of GSI and it is dealt with by using effective stress analysis.	SURFACE CONDITIONS OF DISCONTINUITIES (Predominantly bedding planes) VERY GOOD - Very Rough, fresh unweathered surfaces GOOD - Rough, slightly weathered surfaces FAIR - Smooth, moderately weathered and altered surfaces POOR - Very smooth, occasionally slickensided surfaces with compact coatings or fillings with angular fragments VERY POOR - Very smooth, slickensided or highly weathered surfaces with soft clay coatings or fillings	COMPOSITION AND STRUCTURE A. Thick bedded, very blocky sandstone The effect of pelitic coatings on the bedding planes is minimized by the confinement of the rock mass. In shallow tunnels or slopes these bedding planes may cause structurally controlled instability. B. Sandstone with thin inter-layers of siltstone C. Sandstone and siltstone in similar amounts D. Siltstone or silty shale with sandstone layers E. Weak siltstone or clayey shale with sandstone layers C, D, E, and G - may be more or less folded than illustrated but this does not change the strength. Tectonic deformation, faulting and loss of continuity moves these categories to F and H. F. Tectonically deformed, intensively folded/faulted, sheared clayey shale or siltstone with broken and deformed sandstone layers forming an almost chaotic structure G. Undisturbed silty or clayey shale with or without a few very thin sandstone layers H. Tectonically deformed silty or clayey shale forming a chaotic structure with pockets of clay. Thin layers of sandstone are transformed into small rock pieces. ➡ Means deformation after tectonic disturbance	70 60 50 40 30 20 10
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NC DOT BORE DOUBLE 04 GEO BRDG463 GTM.GPJ NC DOT GDT 12/5/25

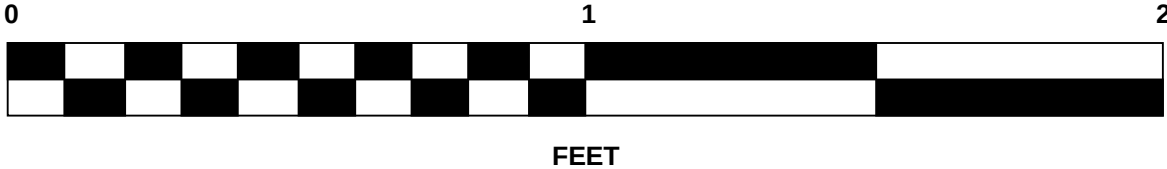
NC DOT BORE DOUBLE 04 GEO_BRDG463_GTM.GPJ NC_DOT.GDT 12/5/25

GEOTECHNICAL BORING REPORT
BORE LOG

WBS 50720.1.1			TIP HB-0050			COUNTY ASHE			GEOLOGIST P. McKenzie						
SITE DESCRIPTION Replace Bridge No. 463 on SR 1563 (Clifton Road) over North Fork New River											GROUND WTR (ft)				
BORING NO. EB1-B			STATION 14+98			OFFSET 18 ft RT			ALIGNMENT -L-		0 HR.	19.6			
COLLAR ELEV. 2,528.9 ft			TOTAL DEPTH 24.6 ft			NORTHING 1,012,745			EASTING 1,298,538		24 HR.	12.0			
DRILL RIG/HAMMER EFF./DATE CG20446 Diedrich D-50 97% 04/30/2024						DRILL METHOD H.S. Augers				HAMMER TYPE Automatic					
DRILLER C. Odom			START DATE 10/14/25			COMP. DATE 10/14/25			SURFACE WATER DEPTH N/A						
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	MOI	L O G	SOIL AND ROCK DESCRIPTION	
			0.5ft	0.5ft	0.5ft	0	25	50	75	100				ELEV. (ft)	DEPTH (ft)
2530															
2525	2,526.1	2.8	4	4	5						M		2,528.9 GROUND SURFACE 0.0		
	2,524.1	4.8	4	7	23								2,522.4 6.5		
2520	2,521.1	7.8	18	36	29						M		Very Dense, Brown, Fine to Coarse Gravelly SAND (A-1-b), with trace mica		
	2,519.1	9.8	26	24	55								2,514.1 14.8		
2515	2,514.1	14.8	32	68	0.4						M			WEATHERED ROCK Brown, (Biotite Granitic Gneiss) 14.8	
2510	2,509.1	19.8	20	17	71						M		2,510.9 RESIDUAL 18.0		
2505	2,504.3	24.6												Hard, Brown, Fine Sandy SILT (A-4), with trace to little mica	
			60	0.0										2,504.3 24.6	
														Boring Terminated with Standard Penetration Test Refusal at Elevation 2,504.3 ft On Crystalline Rock (Biotite Granitic Gneiss)	
														Note: Possible cobbles and boulders in upper 12 feet of Artificial Fill.	

NCDOT BORE DOUBLE 04_GEO_BRDG463_GTM.GPJ NC_DOT.GDT 12/5/25

Replace Bridge No. 463 on SR 1563 (Clifton Road)
over North Fork New River
Ashe County, North Carolina
Rock Core Photographs
B2-A
5.9 to 20.5 Feet



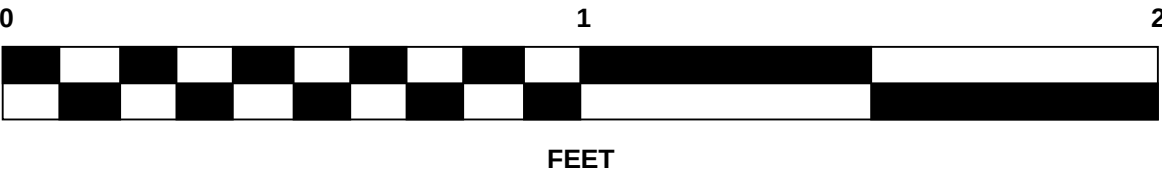
NCDOT BORE DOUBLE 04 GEO BRDG463 GTM.GPJ NC_DOT.GDT 12/4/25

GEOTECHNICAL BORING REPORT

CORE LOG

NCDOT CORE DOUBLE 04 GEO BRDG463 GTM.GPJ NC DOT.GDT 12/4/25

Replace Bridge No. 463 on SR 1563 (Clifton Road)
over North Fork New River
Ashe County, North Carolina
Rock Core Photographs
B2-B
7.6 to 25.1 Feet



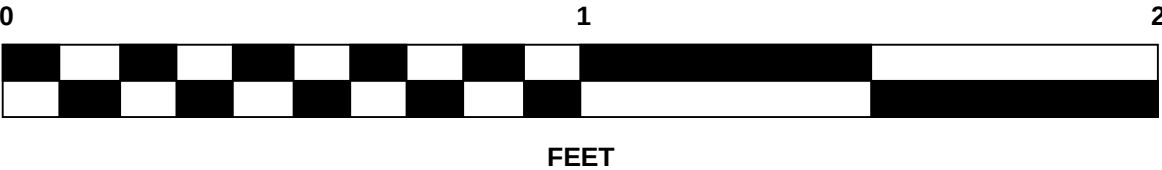
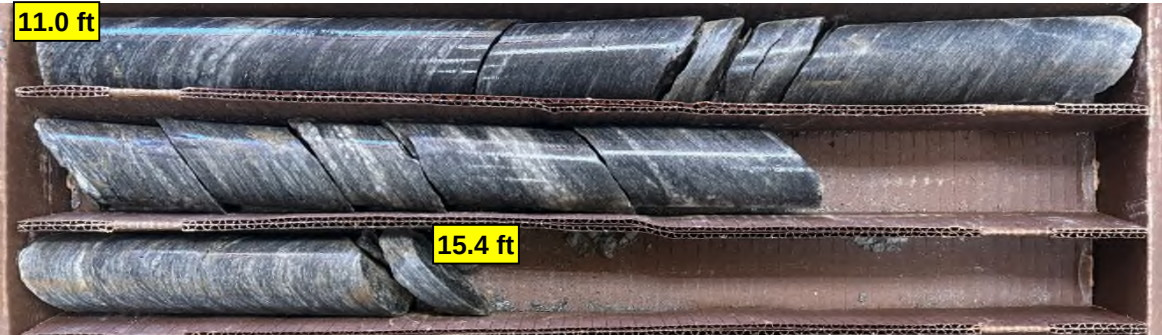
NCDOT BORE DOUBLE 04 GEO BRDG463 GTM.GPJ NC DOT GDT 12/5/25

GEOTECHNICAL BORING REPORT

CORE LOG

NCDOT CORE DOUBLE 04 GEO BRDG463 GTM.GPJ NC_DOT_GDT 12/5/25

Replace Bridge No. 463 on SR 1563 (Clifton Road)
over North Fork New River
Ashe County, North Carolina
Rock Core Photographs
EB2-A
11.0 to 15.4 Feet



GEOTECHNICAL BORING REPORT
BORE LOG

WBS 50720.1.1				TIP HB-0050		COUNTY ASHE		GEOLOGIST P. McKenzie					
SITE DESCRIPTION Replace Bridge No. 463 on SR 1563 (Clifton Road) over North Fork New River										GROUND WTR (ft)			
BORING NO. EB2-B			STATION 17+08			OFFSET 18 ft RT		ALIGNMENT -L-		0 HR.	N/A		
COLLAR ELEV. 2,520.6 ft			TOTAL DEPTH 14.0 ft			NORTHING 1,012,793		EASTING 1,298,742		24 HR.	Caved		
DRILL RIG/HAMMER EFF./DATE CG20446 Diedrich D-50 97% 04/30/2024						DRILL METHOD NW Casing w/ SPT			HAMMER TYPE Automatic				
DRILLER C. Odom			START DATE 10/15/25			COMP. DATE 10/15/25		SURFACE WATER DEPTH N/A					
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG	SOIL AND ROCK DESCRIPTION ELEV. (ft) DEPTH (ft)
			0.5ft	0.5ft	0.5ft	0	25	50	75	100			
2525													
2520	2,520.6	0.0											2,520.6 GROUND SURFACE 0.0
			WOH	1	1								ALLUVIAL Very Loose, Brown, Fine to Coarse Gravelly Sand (A-1-b), with trace mica
2515	2,516.5	4.1	100/0.5										2,514.6 Alluvial Cobbles from 0.0' to 6.0' 6.0
													RESIDUAL Brown, Fine Sandy SILT (A-4), with trace mica
2510	2,511.5	9.1	100/0.3										2,511.5 9.1
													WEATHERED ROCK Gray, (Biotite Granitic Gneiss)
	2,506.6	14.0	60/0.0										2,506.6 14.0
													Boring Terminated with Standard Penetration Test Refusal at Elevation 2,506.6 ft On Crystalline Rock (Biotite Granitic Gneiss)

GEOTECHNICAL BORING REPORT
BORE LOG

SHEET 12

WBS 50720.1.1				TIP HB-0050				COUNTY ASHE				GEOLOGIST P. McKenzie					
SITE DESCRIPTION Replace Bridge No. 463 on SR 1563 (Clifton Road) over North Fork New River												GROUND WTR (ft)					
BORING NO. L_1850L				STATION 18+52				OFFSET 6 ft LT				ALIGNMENT -L-				0 HR. 10.9	
COLLAR ELEV. 2,528.0 ft				TOTAL DEPTH 16.4 ft				NORTHING 1,012,807				EASTING 1,298,881				24 HR. 11.0	
DRILL RIG/HAMMER EFF./DATE CG20446 Diedrich D-50 97% 04/30/2024								DRILL METHOD H.S. Augers				HAMMER TYPE Automatic					
DRILLER C. Odom				START DATE 10/14/25				COMP. DATE 10/14/25				SURFACE WATER DEPTH N/A					
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION			
			0.5ft	0.5ft	0.5ft	0	25	50	75	100				ELEV. (ft)	DEPTH (ft)		
2530																	
														2,528.0	GROUND SURFACE 0.0		
2525	2,526.0	2.0		2	4	3										ROADWAY EMBANKMENT	
															Medium Stiff, Brown, Fine Sandy SILT (A-4), with trace mica		
	2,523.1	4.9		2	2	3							M		2,524.0	Medium Stiff, Brown, Silty CLAY (A-7) 4.0	
2520	2,521.0	7.0		5	18	14							M		2,521.0	Medium Dense, Brown-Gray, Silty Fine to Coarse SAND (A-2-4), with trace to little mica and gravel 7.0	
	2,518.1	9.9		8	12	12									2,517.0	RESIDUAL 11.0	
															Very Stiff, Brown-Orange, Fine Sandy SILT (A-4), with trace mica and gravel		
2515																	
	2,513.1	14.9		20	12	17							M		2,511.6	Boring Terminated at Elevation 2,511.6 ft In Residual Sandy SILT (A-4) 16.4	

NCDOT BORE DOUBLE 04_GEO_BRDG463_GTM.GPJ NC_DOT.GDT 12/5/25

NCDOT BORE DOUBLE 04_GEO_BRDG463_GTM.GPJ NC_DOT.GDT 12/5/25

GEOTECHNICAL BORING REPORT

BORE LOG

WBS 50720.1.1			TIP HB-0050			COUNTY ASHE			GEOLOGIST P. McKenzie						
SITE DESCRIPTION Replace Bridge No. 463 on SR 1563 (Clifton Road) over North Fork New River									GROUND WTR (ft)						
BORING NO. L_2000L			STATION 19+87			OFFSET 14 ft LT			ALIGNMENT -L-			0 HR. Dry			
COLLAR ELEV. 2,534.5 ft			TOTAL DEPTH 16.0 ft			NORTHING 1,012,792			EASTING 1,299,016			24 HR. Dry			
DRILL RIG/HAMMER EFF./DATE CG20446 Diedrich D-50 97% 04/30/2024						DRILL METHOD H.S. Augers			HAMMER TYPE Automatic						
DRILLER C. Odom			START DATE 10/14/25			COMP. DATE 10/14/25			SURFACE WATER DEPTH N/A						
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION	
			0.5ft	0.5ft	0.5ft	0	25	50	75	100				ELEV. (ft)	DEPTH (ft)
2535															
	2,532.3	2.2												2,534.5	0.0
														ROADWAY EMBANKMENT	
														Medium Stiff, Brown, Silty CLAY (A-7), with trace gravel	
2530	2,530.0	4.5													
	2,527.3	7.2												2,528.0	6.5
														Medium Stiff, Brown, Fine Sandy SILT (A-4), with trace mica	
2525	2,525.0	9.5													
														2,521.5	13.0
2520	2,520.0	14.5													
														2,518.5	16.0
														RESIDUAL	
														Hard, Brown-Gray, Fine Sandy SILT (A-4), with trace mica	
														Boring Terminated at Elevation 2,518.5 ft In Residual Sandy SILT (A-4)	
														Note: Surficial Organic Laden Soil: 0.0-0.3 ft.	
														Possible cobbles and boulders from 12 to 13 feet in the Roadway Embankment.	

ROCK TEST RESULTS									
SAMPLE NO.	BORING	NORTHING	EASTING	STATION	OFFSET	DEPTH INTERVAL	ROCK TYPE	UNIT WEIGHT (PCF)	UNCONFINED COMPRESSIVE STRENGTH
RS-01	B2-A	1012805	1298670	16 + 42 -L-	10' LT	5.9'-6.5'	BIOTITE GRANITIC GNEISS	171.6	2,560 psi / 369 ksf
RS-02	B2-B	1012778	1298671	16 + 35 -L-	17' RT	16.9'-17.6'	BIOTITE GRANITIC GNEISS	175.4	4,160 psi / 599 ksf

Alex M. Atkinson

AUTHORIZED SIGNATURE
NCDOT CERT NO. 130-04-0212

Prepared in the Office of:
F&ME CONSULTANTS, INC.
COLUMBIA, SOUTH CAROLINA
NCDOT LAB CERT. NO. 130-0212

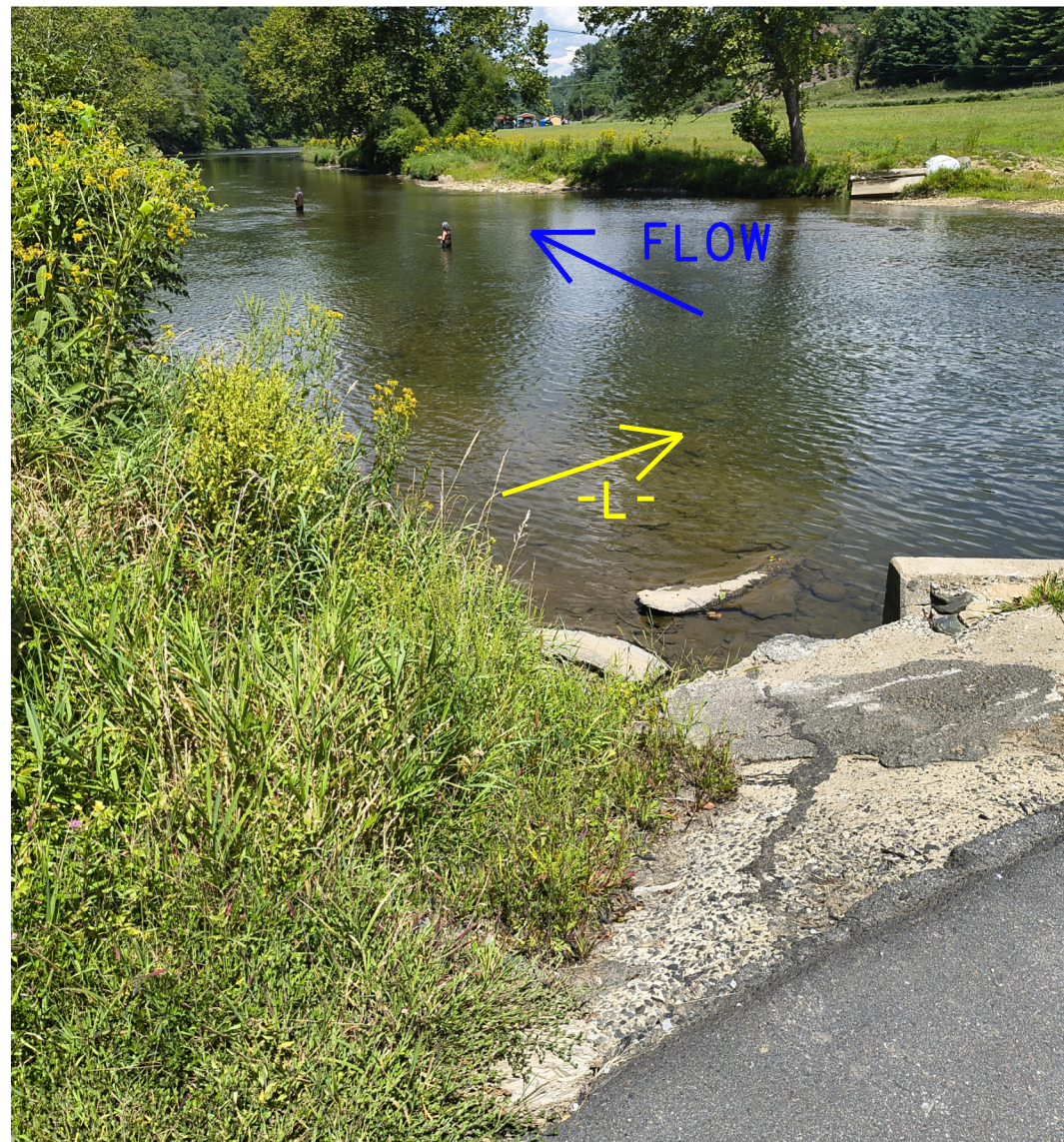


PHOTO #1: VIEW FACING NORTH, DOWNSTREAM.



PHOTO #2: VIEW FROM END BENT NO. 1 FACING EAST TOWARD END BENT 2.

REFERENCE: HB-0053

PROJECT: 50723

CONTENTS

SHEET NO.	DESCRIPTION
I	TITLE SHEET
2	LEGEND (SOIL & ROCK)
2A	SUPPLEMENTAL LEGEND (GSI)
3	SITE PLAN
4-9	BORE LOGS, CORE REPORTS, & CORE PHOTOS
10	ROCK TEST RESULTS
II	SITE PHOTOGRAPHS

STATE OF NORTH CAROLINA
DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT

STRUCTURE
SUBSURFACE INVESTIGATION

COUNTY ASHE

PROJECT DESCRIPTION REPLACE BRIDGE NO. 480 ON
SR 1126 (ED LITTLE ROAD) OVER NORTH FORK
NEW RIVER

SITE DESCRIPTION BRIDGE NO. 0480

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	HB-0053	1	

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- NOTES:
- THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE N.C. DEPARTMENT OF TRANSPORTATION AS ACCURATE NOR IS IT CONSIDERED PART OF THE PLANS, SPECIFICATIONS OR CONTRACT FOR THE PROJECT.
 - BY HAVING REQUESTED THIS INFORMATION, THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

PERSONNEL

CG2 EXPLORATION

K. CLARK

INVESTIGATED BY CG2, PLLC

DRAWN BY M. MALISHER, E.I.T.

CHECKED BY M. WALKO, P.E.

SUBMITTED BY CG2, PLLC

DATE JANUARY 2026

Prepared in the Office of:



CAROLINAS
GEOTECHNICAL
GROUP

1805 SARDIS ROAD N
SUITE 100
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(980) 339-8684



Signed by: Michael J. Walko 01/13/2026

42C082874D56441C SIGNATURE DATE

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NORTH CAROLINA DEPARTMENT OF TRANSPORTATION

DIVISION OF HIGHWAYS

GEOTECHNICAL ENGINEERING UNIT

SUBSURFACE INVESTIGATION

SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

SOIL DESCRIPTION										GRADATION										ROCK DESCRIPTION										TERMS AND DEFINITIONS																													
SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 206, ASTM D1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE, <i>VERY STIFF, GRAY, SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6</i>										WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE. UNIFORMLY GRADED - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE. GAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.										HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED. AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL. THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:										ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER. AQUIFER - A WATER BEARING FORMATION OR STRATA. ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND. ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC. ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE. CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE. COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE. CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK. DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL. DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH. FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE. FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES. FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLOGGED FROM PARENT MATERIAL. FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM. FORMATION (FM.) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD. JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED. LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT. LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS. MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE. PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM. RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK. ROCK QUALITY DESIGNATION (RQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK. SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS. SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE. STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS (N OR BPF) OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS. STRATA CORE RECOVERY (SREC) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE. STRATA ROCK QUALITY DESIGNATION (SROQ) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE. TOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.																													
SOIL LEGEND AND AASHTO CLASSIFICATION										ANGULARITY OF GRAINS										WEATHERED ROCK (WR)										NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT N VALUES > 100 BLOWS PER FOOT IF TESTED.																													
GENERAL CLASS.		GRANULAR MATERIALS (≤ 35% PASSING #200)					SILT-CLAY MATERIALS (> 35% PASSING #200)					ORGANIC MATERIALS					CRYSTALLINE ROCK (CR)		FINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES GRANITE, GNEISS, GABBRO, SCHIST, ETC.																																								
GROUP CLASS.		A-1-a		A-1-b		A-3		A-2-4		A-2		A-2-6		A-2-7		A-4		A-5		A-6		A-7		A-1, A-2 A-3		A-4, A-5 A-6, A-7																																	
SYMBOL																																																											
% PASSING		#10		#40		#200																				GRANULAR SOILS		SILT-CLAY SOILS		MUCK, PEAT																													
MATERIAL PASSING #40		LL		PI																								SOILS WITH LITTLE OR MODERATE AMOUNTS OF ORGANIC MATTER		HIGHLY ORGANIC SOILS																													
GROUP INDEX		0		0		0		4 MX		8 MX		12 MX		16 MX		NO MX																																											
USUAL TYPES OF MAJOR MATERIALS		STONE FRAGS, GRAVEL, AND SAND		FINE SAND		SILTY OR CLAYEY GRAVEL AND SAND				SILTY SOILS		CLAYEY SOILS																																															
GEN. RATING AS SUBGRADE		EXCELLENT TO GOOD					FAIR TO POOR					FAIR TO POOR					POOR					UNSUITABLE																																					
PI OF A-7-5 SUBGROUP IS ≤ LL - 30; PI OF A-7-6 SUBGROUP IS > LL - 30																																																											
CONSISTENCY OR DENSENESS										MISCELLANEOUS SYMBOLS										ROCK HARDNESS										FRACTURE SPACING																													
PRIMARY SOIL TYPE		COMPACTNESS OR CONSISTENCY		RANGE OF STANDARD PENETRATION RESISTANCE (N-VALUE)		RANGE OF UNCONFINED COMPRESSIVE STRENGTH (TONS/FT ²)																																																					
GENERAL		VERY LOOSE		< 4		N/A																																																					
GENERAL		LOOSE		4 TO 10																																																							
GENERAL		MEDIUM DENSE		10 TO 30																																																							
GENERAL		DENSE		30 TO 50																																																							
GENERAL		VERY DENSE		> 50																																																							
GENERAL		VERY SOFT		2 TO 4		< 0.25																																																					
GENERAL		SOFT		4 TO 8		0.25 TO 0.5																																																					
GENERAL		MEDIUM STIFF		8 TO 15		0.5 TO 1.0																																																					
GENERAL		STIFF		15 TO 30		1 TO 2																																																					
GENERAL		VERY STIFF		> 30		2 TO 4																																																					
GENERAL		HARD		> 30		> 4																																																					
TEXTURE OR GRAIN SIZE										RECOMMENDATION SYMBOLS										ROCK HARDNESS										BEDDING																													
U.S. STD. SIEVE SIZE		4		10		40		60		200		270																																															
OPENING (MM)		4.76		2.00		0.42		0.25		0.075		0.053																																															
BOULDER (BLDR.)		COBBLE (COB.)		GRAVEL (GR.)		COARSE SAND (CSE, SD.)		FINE SAND (F SD.)		SILT (SL.)		CLAY (CL.)																																															
GRAIN SIZE		305		75		2.0		0.25		0.05		0.005																																															
MM		IN.																																																									
SOIL MOISTURE - CORRELATION OF TERMS										ABBREVIATIONS										ROCK HARDNESS										BEDDING																													
SOIL MOISTURE SCALE (ATTERBERG LIMITS)		FIELD MOISTURE DESCRIPTION		GUIDE FOR FIELD MOISTURE DESCRIPTION																																																							
LL		LIQUID LIMIT		USUALLY LIQUID; VERY WET, USUALLY FROM BELOW THE GROUND WATER TABLE																																																							
PLASTIC RANGE (PI)		PLASTIC LIMIT		SEMISOLID; REQUIRES DRYING TO ATTAIN OPTIMUM MOISTURE																																																							
OM		OPTIMUM MOISTURE		SOLID; AT OR NEAR OPTIMUM MOISTURE																																																							
SL		SHRINKAGE LIMIT		REQUIRES ADDITIONAL WATER TO ATTAIN OPTIMUM MOISTURE																																																							
DRY - (ID)																																																											
PLASTICITY										EQUIPMENT USED ON SUBJECT PROJECT										ROCK HARDNESS										BEDDING																													
PLASTICITY INDEX (PI)		DRY STRENGTH																																																									
NON PLASTIC		0-5		VERY LOW																																																							
SLIGHTLY PLASTIC		6-15		SLIGHT																																																							
MODERATELY PLASTIC		16-25		MEDIUM																																																							
HIGHLY PLASTIC		26 OR MORE		HIGH																																																							
COLOR										EQUIPMENT USED ON SUBJECT PROJECT										ROCK HARDNESS										BEDDING																													
DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY). MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.										DRILL UNITS:										ADVANCING TOOLS:										HAMMER TYPE:										CORE SIZE:																			
										☐ CME-45C										☐ CLAY BITS										☒ AUTOMATIC										☐ MANUAL																			
										☐ CME-55										☐ 6" CONTINUOUS FLIGHT AUGER										☐ CORE SIZE:										☐ -B																			
										☐ CME-550										☐ 8" HOLLOW AUGERS										☐ -H																													
										☐ VANE SHEAR TEST										☐ HARD FACED FINGER BITS										☐ TUNG.-CARBIDE INSERTS										☒ N-Q																			
										☐ PORTABLE HOIST										☒ CASING										☒ W/ ADVANCER										☐ HAND TOOLS:																			
										☒ DIEDRICH D-50										☐ TRICONE										☐ * STEEL TEETH										☐ POST HOLE DIGGER																			
										☐										☐ TRICONE										☐ * TUNG.-CARB.										☐ HAND AUGER																			
										☐										☒ CORE BIT										☐										☐ SOUNDING ROD																			
										☐										☐										☐										☐ VANE SHEAR TEST																			
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NORTH CAROLINA DEPARTMENT OF TRANSPORTATION

DIVISION OF HIGHWAYS

GEOTECHNICAL ENGINEERING UNIT

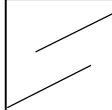
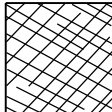
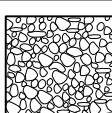
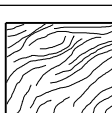
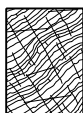
SUBSURFACE INVESTIGATION

SUPPLEMENTAL LEGEND, GEOLOGICAL STRENGTH INDEX (GSI) TABLES

FROM AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS

AASHTO LRFD Figure 10.4.6.4-1 — Determination of GSI for Jointed Rock Mass (Marinos and Hoek, 2000)

AASHTO LRFD Figure 10.4.6.4-2 — Determination of GSI for Tectonically Deformed Heterogeneous Rock Masses (Marinos and Hoek, 2000)

GEOLOGICAL STRENGTH INDEX (GSI) FOR JOINTED ROCKS (Hoek and Marinos, 2000) From the lithology, structure and surface conditions of the discontinuities, estimate the average value of GSI. Do not try to be too precise. Quoting a range from 33 to 37 is more realistic than stating that GSI = 35. Note that the table does not apply to structurally controlled failures. Where weak planar structural planes are present in an unfavorable orientation with respect to the excavation face, these will dominate the rock mass behaviour. The shear strength of surfaces in rocks that are prone to deterioration as a result of changes in moisture content will be reduced if water is present. When working with rocks in the fair to very poor categories, a shift to the right may be made for wet conditions. Water pressure is dealt with by effective stress analysis.		SURFACE CONDITIONS VERY GOOD Very rough, fresh unweathered surfaces GOOD Rough, slightly weathered, iron stained surfaces FAIR Smooth, moderately weathered and altered surfaces POOR Slickensided, highly weathered surfaces with compact coatings or fillings or angular fragments VERY POOR Slickensided, highly weathered surfaces with soft clay coatings or fillings		DECREASING SURFACE QUALITY		GSI FOR HETEROGENEOUS ROCK MASSES SUCH AS FLYSCH (Marinos, P and Hoek E., 2000) From a description of the lithology, structure and surface conditions (particularly of the bedding planes), choose a box in the chart. Locate the position in the box that corresponds to the condition of the discontinuities and estimate the average value of GSI from the contours. Do not attempt to be too precise. Quoting a range from 33 to 37 is more realistic than giving GSI = 35. Note that the Hoek-Brown criterion does not apply to structurally controlled failures. Where unfavourably oriented continuous weak planar discontinuities are present, these will dominate the behaviour of the rock mass. The strength of some rock masses is reduced by the presence of groundwater and this can be allowed for by a slight shift to the right in the columns for fair, poor and very poor conditions. Water pressure does not change the value of GSI and it is dealt with by using effective stress analysis.		SURFACE CONDITIONS OF DISCONTINUITIES (Predominantly bedding planes) VERY GOOD - Very Rough, fresh unweathered surfaces GOOD - Rough, slightly weathered surfaces FAIR - Smooth, moderately weathered and altered surfaces POOR - Very smooth, occasionally slickensided surfaces with compact coatings or fillings with angular fragments VERY POOR - Very smooth, slicken-sided or highly weathered surfaces with soft clay coatings or fillings	
STRUCTURE						COMPOSITION AND STRUCTURE			
 INTACT OR MASSIVE - intact rock specimens or massive in situ rock with few widely spaced discontinuities  BLOCKY - well interlocked undisturbed rock mass consisting of cubical blocks formed by three intersecting discontinuity sets  VERY BLOCKY - interlocked, partially disturbed mass with multi-faceted angular blocks formed by 4 or more joint sets  BLOCKY/DISTURBED/SEAMY - folded with angular blocks formed by many intersecting discontinuity sets. Persistence of bedding planes or schistosity  DISINTEGRATED - poorly interlocked, heavily broken rock mass with mixture of angular and rounded rock pieces  LAMINATED/SHEARED - Lack of blockiness due to close spacing of weak schistosity or shear planes		DECREASING INTERLOCKING OF ROCK PIECES		90 80 70 60 50 40 30 20 10 N/A N/A		 A. Thick bedded, very blocky sandstone The effect of pelitic coatings on the bedding planes is minimized by the confinement of the rock mass. In shallow tunnels or slopes these bedding planes may cause structurally controlled instability.  B. Sandstone with thin inter-layers of siltstone  C. Sandstone and siltstone in similar amounts  D. Siltstone or silty shale with sandstone layers  E. Weak siltstone or clayey shale with sandstone layers  F. Tectonically deformed, intensively folded/faulted, sheared clayey shale or siltstone with broken and deformed sandstone layers forming an almost chaotic structure  G. Undisturbed silty or clayey shale with or without a few very thin sandstone layers  H. Tectonically deformed silty or clayey shale forming a chaotic structure with pockets of clay. Thin layers of sandstone are transformed into small rock pieces. C, D, E, and G - may be more or less folded than illustrated but this does not change the strength. Tectonic deformation, faulting and loss of continuity moves these categories to F and H. Means deformation after tectonic disturbance		70 60 50 40 30 20 10 A B C D E F G H	

DATE: 8-19-16

GEOTECHNICAL BORING REPORT
BORE LOG

WBS 50723.1.1		TIP HB-0053		COUNTY ASHE		GEOLOGIST K. Clark								
SITE DESCRIPTION Replace Bridge No. 480 on SR 1126 (Ed Little Road) over North Fork New River							GROUND WTR (ft)							
BORING NO. EB1-A		STATION 11+79		OFFSET 16 ft LT		ALIGNMENT L		0 HR. N/A						
COLLAR ELEV. 2,796.7 ft		TOTAL DEPTH 23.7 ft		NORTHING 991,849		EASTING 1,234,424		24 HR. 2.4						
DRILL RIG/HAMMER EFF./DATE CG20446 Diedrich D-50 97% 04/30/2024				DRILL METHOD NW Casing w/ SPT			HAMMER TYPE Automatic							
DRILLER C. Odom			START DATE 10/21/25		COMP. DATE 10/21/25		SURFACE WATER DEPTH N/A							
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT			SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION	DEPTH (ft)	
			0.5ft	0.5ft	0.5ft	0	25	50	75	100				
2800														
	2,796.7	0.0											2,796.7	0.0
2795			1	2	6								2,794.2	2.5
	2,793.0	3.7												
2790			3	4	5									
	2,788.0	8.7												
2785			48	48	29									
	2,783.0	13.7											2,783.0	13.7
2780			54	46/0.4										
	2,778.0	18.7											2,779.2	17.5
2775			17	37	58									
	2,773.0	23.7											2,773.0	23.7
			60/0.0											

NCDOT BORE DOUBLE 04_GEO_BRDG480_GTM.GPJ NC_DOT.GDT 12/5/25

GEOTECHNICAL BORING REPORT
BORE LOG

SHEET 4

WBS 50723.1.1		TIP HB-0053		COUNTY ASHE		GEOLOGIST K. Clark								
SITE DESCRIPTION Replace Bridge No. 480 on SR 1126 (Ed Little Road) over North Fork New River							GROUND WTR (ft)							
BORING NO. EB1-B		STATION 11+76		OFFSET 11 ft RT		ALIGNMENT L		0 HR. Dry						
COLLAR ELEV. 2,795.6 ft		TOTAL DEPTH 13.4 ft		NORTHING 991,840		EASTING 1,234,450		24 HR. Dry						
DRILL RIG/HAMMER EFF./DATE CG20446 Diedrich D-50 97% 04/30/2024				DRILL METHOD NW Casing w/ SPT			HAMMER TYPE Automatic							
DRILLER C. Odom			START DATE 10/21/25		COMP. DATE 10/21/25		SURFACE WATER DEPTH N/A							
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT			SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION		
			0.5ft	0.5ft	0.5ft	0	25	50	75	100			ELEV. (ft)	DEPTH (ft)
2800														
2795	2,795.6	0.0											2,795.6	0.0
2790	2,792.2	3.4	3	4	5						M	L	GROUND SURFACE	
	2,792.2	3.4	3	7	7						M		2,793.1	2.5
2785	2,787.2	8.4											2,788.1	7.5
	2,782.2	13.4	21	55	35						M		2,782.2	13.4
			60/0.0										Boring Terminated with Standard Penetration Test Refusal at Elevation 2,782.2 ft On Crystalline Rock (Granitic Gneiss)	

NCDOT BORE DOUBLE 04_GEO_BRDG480_GTM.GPJ NC_DOT.GDT 12/5/25

GEOTECHNICAL BORING REPORT
BORE LOG

WBS 50723.1.1				TIP HB-0053		COUNTY ASHE		GEOLOGIST K. Clark							
SITE DESCRIPTION Replace Bridge No. 480 on SR 1126 (Ed Little Road) over North Fork New River										GROUND WTR (ft)					
BORING NO. B1-A				STATION 12+32		OFFSET 21 ft LT		ALIGNMENT -L-		0 HR.	N/A				
COLLAR ELEV. 2,790.8 ft				TOTAL DEPTH 39.1 ft		NORTHING 991,902		EASTING 1,234,431		24 HR.	Caved				
DRILL RIG/HAMMER EFF./DATE CG20446 Diedrich D-50 97% 04/30/2024						DRILL METHOD NW Casing W/SPT & Core			HAMMER TYPE Automatic						
DRILLER C. Odom				START DATE 10/21/25		COMP. DATE 10/21/25		SURFACE WATER DEPTH 1.0ft							
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION	
			0.5ft	0.5ft	0.5ft	0	25	50	75	100				ELEV. (ft)	DEPTH (ft)
2795															
2790	2,790.8	0.0													
	2,787.2	3.6	2	2	2										
2785			19	35	40										
	2,782.2	8.6													
2780			12	88/0.4											
	2,777.2	13.6													
2775	2,776.5	14.3	60	40/0.2											
			60/0.0												
2770															
											RS-01				
2765															
2760											RS-02				
2755															

GEOTECHNICAL BORING REPORT
CORE LOG

SHEET 5

WBS 50723.1.1				TIP HB-0053		COUNTY ASHE		GEOLOGIST K. Clark							
SITE DESCRIPTION Replace Bridge No. 480 on SR 1126 (Ed Little Road) over North Fork New River										GROUND WTR (ft)					
BORING NO. B1-A				STATION 12+32			OFFSET 21 ft LT		ALIGNMENT -L-		0 HR. N/A				
COLLAR ELEV. 2,790.8 ft				TOTAL DEPTH 39.1 ft			NORTHING 991,902		EASTING 1,234,431		24 HR. Caved				
DRILL RIG/HAMMER EFF./DATE CG20446 Diedrich D-50 97% 04/30/2024							DRILL METHOD NW Casing W/SPT & Core			HAMMER TYPE Automatic					
DRILLER C. Odom				START DATE 10/21/25			COMP. DATE 10/21/25		SURFACE WATER DEPTH 1.0ft						
CORE SIZE NQ				TOTAL RUN 24.8 ft											
ELEV (ft)	RUN ELEV (ft)	DEPTH (ft)	RUN (ft)	DRILL RATE (Min/ft)	RUN REC. (ft) %		RQD (ft) %	SAMP. NO.	STRATA REC. (ft) %		RQD (ft) %	L O G	DESCRIPTION AND REMARKS		DEPTH (ft)
2776.5	2,776.5	14.3	4.8	N=60/0.0 2:34/0.8 2:27/1.0 2:22/1.0 1:54/1.0 1:32/1.0	(2.2) 46%	(1.7) 35%			(22.2) 90%	(21.5) 87%			Begin Coring @ 14.3 ft		
2775													CRYSTALLINE ROCK		14.3
													Slightly Weathered to Fresh, Hard to Very Hard, Gray-White, (Granitic Gneiss), with Very Close to Moderately Close Fracture Spacing		
	2,771.7	19.1											GSI = 70-75		
2770			5.0	2:42/1.0 4:09/1.0 3:20/1.0 3:21/1.0 3:47/1.0	(5.0) 100%	(4.8) 96%							RS-01: 22.3'-22.9' Unit Weight: 170.8 pcf Unconfined Compressive Strength: 9,300 psi (1,340 ksf)		
	2,766.7	24.1						RS-01							
2765			5.0	3:06/1.0 2:18/1.0 2:18/1.0 1:49/1.0 2:25/1.0	(5.0) 100%	(5.0) 100%							RS-02: 32.5'-33.0' Unit Weight: 173.0 pcf Unconfined Compressive Strength: 16,040 psi (2,300 ksf)		
	2,761.7	29.1													
2760			5.0	1:56/1.0 2:06/1.0 2:27/1.0 2:42/1.0 2:16/1.0	(5.0) 100%	(5.0) 100%									
	2,756.7	34.1						RS-02							
2755			5.0	1:56/1.0 2:08/1.0 2:36/1.0 2:25/1.0 3:00/1.0	(5.0) 100%	(5.0) 100%									
	2,751.7	39.1										Boring Terminated at Elevation 2,751.7 ft In Crystalline Rock (Granitic Gneiss)		39.1	

NCDOT BORE DOUBLE HB0053_GEO_BRDG0480_GTM.GPJ NC_DOT.GDT 12/16/25

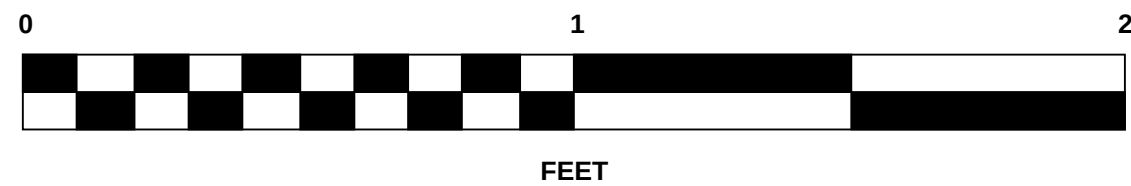
NCDOT BORE DOUBLE HB0053_GEO_BRDG0480_GTM.GPJ NC_DOT.GDT 12/16/25

Replace Bridge No. 480 on SR 1126 (Ed Little Rd) over North Fork New River
Ashe County, North Carolina
Rock Core Photographs
Boring: B1-A
14.3 to 39.1 Feet



WBS 50723.1.1			TIP HB-0053			COUNTY ASHE			GEOLOGIST K. Clark						
SITE DESCRIPTION Replace Bridge No. 480 on SR 1126 (Ed Little Road) over North Fork New River									GROUND WTR (ft)						
BORING NO. B1-B			STATION 12+29			OFFSET 22 ft RT			ALIGNMENT -L-			0 HR. N/A			
COLLAR ELEV. 2,790.0 ft			TOTAL DEPTH 40.3 ft			NORTHING 991,890			EASTING 1,234,472			24 HR. Caved			
DRILL RIG/HAMMER EFF./DATE CG20446 Diedrich D-50 97% 04/30/2024						DRILL METHOD NW Casing W/SPT & Core			HAMMER TYPE Automatic						
DRILLER C. Odom			START DATE 10/22/25			COMP. DATE 10/22/25			SURFACE WATER DEPTH 1.0ft						
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG	SOIL AND ROCK DESCRIPTION		
			0.5ft	0.5ft	0.5ft	0	25	50	75	100				ELEV. (ft)	DEPTH (ft)
2790	2,790.0	0.0	4	13	20									2,790.0	0.0
2785	2,786.2	3.8	13	49	51/0.2									2,785.7	4.3
2780	2,781.2	8.8	100/0.4												
2775	2,776.2	13.8	100/0.2												
2770	2,771.2	18.8	33	24	20									2,773.5	16.5
2765	2,766.2	23.8	60/0.0											2,766.2	23.8
2760											RS-03			2,764.5	25.5
2755															
2750											RS-04			2,749.7	40.3
Boring Terminated at Elevation 2,749.7 ft In Crystalline Rock (Granitic Gneiss)															

**Replace Bridge No. 480 on SR 1126 (Ed Little Rd) over North Fork New River
Ashe County, North Carolina
Rock Core Photographs
Boring: B1-B
25.5 to 40.3 Feet**



ROCK TEST RESULTS									
SAMPLE NO.	BORING	NORTHING	EASTING	STATION	OFFSET	DEPTH INTERVAL	ROCK TYPE	UNIT WEIGHT (PCF)	UNCONFINED COMPRESSIVE STRENGTH
RS-01	B1-A	991902	1234431	12 + 32 -L-	21' LT	22.3'-22.9'	GRANITIC GNEISS	170.8	9,300 psi /1,340 ksf
RS-02	B1-A	991902	1234431	12 + 32 -L-	21' LT	32.5'-33.0'	GRANITIC GNEISS	173.0	16,040 psi /2,300 ksf
RS-03	B1-B	991890	1234472	12 + 29 -L-	22' RT	27.5'-28.2'	GRANITIC GNEISS	176.9	23,340 psi /3,360 ksf
RS-04	B1-B	991890	1234472	12 + 29 -L-	22' RT	36.5'-37.2'	GRANITIC GNEISS	172.0	10,670 psi /1,530 ksf

	119-0705
	NCDOT Cert. No.
	10/16/25
Authorized Signature	Date

Prepared in the Office of:
UES
PINEVILLE, NC
NCDOT LAB CERT. NO. 119-0705



PHOTO #1: VIEW FROM END BENT NO. 2 FACING SOUTH TOWARD END BENT NO. 1.



PHOTO #2: VIEW FROM END BENT NO. 1 FACING NORTH, UPSTREAM.